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Energy Management Strategies for Fuel Cell Hybrid Vehicles; an Overview

Edwin Tazelaar¹, Bram Veenhuizen¹, José Jagerman¹, Ton Faassen¹

**IEdwin Tazelaar (corresponding author), HAN University of Applied Sciences,

Arnhem, the Netherlands, e.tazelaar@han.nl

Abstract

For proper operation, fuel cell hybrid propulsion systems need an Energy Management Strategy (EMS). A variety of such EMSs have been presented in literature. This paper provides an overview of EMSs recently proposed in literature. It categorizes the EMSs to their theoretical background, their applicability to different electric topologies, the storage technology used and the considered vehicle type. From this inventory is concluded that for a broad range of topologies for PEM-based fuel cell hybrid propulsion systems, EMSs are available in literature. Issues left for further scientific research are the further exploration how to integrate a-priori information as trip data in the EMS and how to expand the lifetime of the fuel cell stack and/or the storage by including models and measures against degradation in an optimizing EMS. Issues left for practical implementation are an extension of the area of operation to harsh environments and cold startups and a real-time validation of proposed EMSs on actual fuel cell hybrid vehicles.

Fuel Cell Hybrid Vehicle, Energy Management Strategy, Control Theory

1 Introduction

1.1 Background

Hybrid propulsion systems by definition comprise a primary power source and an energy storage. For Fuel Cell Hybrid Electric Vehicles (FCHEV), the fuel cell system acts as the primary source and a battery and/or supercapacitor enables the storage of electrical energy. As both the primary source and the storage can provide electric power for propulsion, a control strategy is needed to define the distribution of this power demand over fuel cell stack and storage. In literature, this supervisory control strategy is referred to as the power split strategy, power split control, power management strategy or energy management strategy. In this paper it will be referred to as the Energy Management Strategy (EMS). The EMS has to ensure that constraints on the operation of the fuel cell system and storage are not violated, without compromising on the drivability of the vehicle. Main constraints to be consid-

ered are the power ratings of fuel cell stack and storage and the prevention of depletion or over-charging the storage. As not violating these constraints does not result in one unique solution, it leaves the EMS room for optimization. This free-dom in the control problem is reflected in the variety of EMSs presented in literature.

1.2 Objective

This paper intends to provide an overview of EMSs for fuel cell hybrid propulsion systems discussed in literature. Objective of this overview is to enable the reader to decide which literature to examine in support of own EMS development and implementation.

1.3 Approach

Based on a literature survey over journals of publishers as Elsevier, IEEE and Springer, and conferences regarding fuel cell hybrid propulsion,

recent developments in EMSs for FCHEVs have been evaluated. These results are merged with the observations made in a PhD project on energy management for hybrid propulsion systems [86].

2 Publications

Clearly, energy management for fuel cell hybrid propulsion is a recent area of scientific research. Although both fuel cell technology and control and optimization theory exists for over at least five decades, the vast majority of publications on the subject are presented only in the last ten years (figure 1). This is in line with the recent awareness for sustainable transportation.

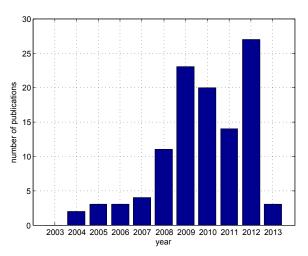


Figure 1: Publications per year.

With respect to publications, it is remarkable that first authors countries, contributing most to EMS solutions for fuel cell hybrid propulsion, are not necessarily countries with a traditional large automotive industry (see figure 2). Countries with a modest automotive industry, as Canada and Spain, do significantly contribute to this subject. For Canada, this can be partly understood from their leading fuel cell industry. More remarkable is that countries like Germany and Japan, with a strong automotive industry, appear to have no significant contribution on the subject.

3 Vehicles

Most publications on EMSs for FCHEVs do not state to which vehicle type the presented EMS applies. Therefore, most EMSs can be considered sufficiently generic to be relevant to a broad variety of vehicle types.

Nevertheless, a few papers consider a specific type of vehicle, such as a three-wheel auto rickshaw [62], a scooter [48, 83], an unmanned ground combat vehicle [1], a low speed cargo vehicle [26, 67], a city bus [33, 57, 95, 102, 103,

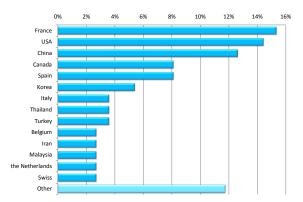


Figure 2: Publications found, categorized per first authors country.

104], a tramway [29, 34, 93, 95] and a specialized test vehicle [63]. Although specific in vehicle type, most of these papers can be considered a demonstration of a generic EMS on a specific vehicle. This further supports the statement that most presented EMSs are sufficiently generic to be applicable to different vehicle types.

In addition, some papers also consider stationary back-up systems [95] and grid connected systems including a reformer [37], extending the application of the EMS to more than vehicles.

4 Topologies

As primary power source, generally Polymer Electrolyte Membrane (PEM) fuel cells are considered. For propulsion, PEM technology is that common, that the majority of publications just refer to fuel cells, even when considering only PEM fuel cells. A few publications explicitly consider different fuel cell technologies, as High Temperature PEM ([46]) and a fuel cell system including a reformer [37]. Although the characterization of these fuel cell technologies for EMS differs slightly from PEM, the EMSs presented for specific fuel cell technologies should not be considered very different from those considering low temperature, direct hydrogen PEM.

With respect to the storage of electrical energy, two main groups can be distinguished: EMSs that consider a battery and EMSs that consider a supercapacitor or ultra-capacitor as storage, as indicated in figure 3. A minority considers the combination of both a battery and a supercapacitor, or more than one storage configuration, including no storage at all.

When defined, the battery technology considered is dominantly lithium-ion.

All EMSs consider the amount of stored energy. From the perspective of the EMS, a supercapacitor has the advantage over a battery that the amount of stored energy is directly indicated by the voltage on its terminals, whereas for batteries, most EMSs assume a State Of Charge (SOC) or State Of Energy (SOE) estimator to identify the

amount of stored energy, without further specification.

The electric motor(s) of the vehicle are connected by an inverter to the DC-bus of the propulsion system. The fuel cell stack and the battery and/or supercapacitor as storage can be electrically connected to this DC-bus in several topologies. Figure 4 indicates some of these configurations.

- Topology (1) combines fuel cell stack and storage without any DC/DC converter. In this configuration, the power delivered by the fuel cell stack and the battery or supercapacitor are directly coupled. A reference to this configuration is rare [7].
- Topology (2) is a common configuration. It enables the control of the power split over the fuel cell stack and the battery. This configuration is referred to in [1, 6, 14, 17, 21, 22, 27, 28, 32, 36, 40, 45, 47, 49, 50, 51, 54, 56, 57, 58, 59, 61, 62, 65, 69, 75, 77, 78, 80, 81, 82, 83, 84, 85, 86, 93, 99, 100, 101, 102, 103, 104, 108].
- As the DC/DC converter in topology (3) is more complex (bidirectional) as in topology (2) and as energy from the storage will always pass the converter twice (charging/discharging), this topology is not favorable with respect to power electronics and losses. It is referred to in [16, 74, 96] and to some extent in [73].
- Topology (4) is commonly supported. This configuration enables the control of both fuel cell stack power and the power from the storage. As these powers should match the demanded power, a tight control of both converters is needed. An additional capacitor on the DC-bus to decouple fuel cell stack and storage power from the power demand relaxes this problem, but essentially, this results in topology (5). Configuration (4) enables the control of the DC-bus voltage, prohibiting large voltage swings on the

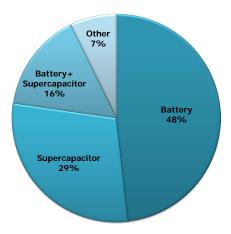


Figure 3: Energy storage.

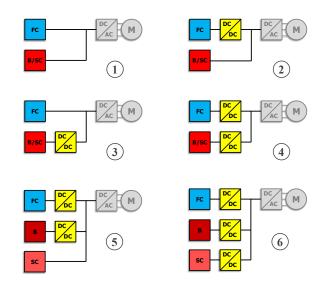


Figure 4: Topologies.

DC-bus. As a result, the inverter requirements on its DC-voltage can be less stringent. A few publications, as [38], discuss the topology on voltage level. Most publications only consider power flows, and do not further elucidate the subject. It is referred to in [2, 3, 5, 10, 12, 23, 30, 31, 34, 35, 37, 44, 41, 52, 53, 55, 60, 63, 64, 72, 79, 87, 88, 91, 92, 94, 97, 110, 112].

- Topology (5) includes both a battery and a supercapacitor as storage. Advantage of this configuration is the combination of the power handling capabilities of the supercapacitor with the energy storage capabilities of the battery. Disadvantage is its complexity. Disadvantage is its complexity. It is referred to in [33, 64]. This configuration, but with the battery and supercapacitor interchanged, is mentioned in [58].
- For topology (6), comprising a fuel cell stack, battery and supercapacitor, DC/DC converters are included between all components and the DC-bus [25, 66, 68, 89, 98, 105, 107]. As topology (5), it combines the advantage of the power handling capabilities of the supercapacitor with the energy storage capabilities of the battery. Comparable to topology (4) over (3), it enables voltage control of the DC-bus, but all against an increase in complexity.

A number of less frequent mentioned alternative topologies are reported. Some examples of variations mentioned:

• In [48] an integrated power electronics solution is presented for a relative low power application, combining the power flow of the fuel cell stack and supercapacitor in one converter structure.

- As alternative topology, [9] proposes to charge the battery from the fuel cell stack using a separate DC/DC converter, with a diode connection to the supercapacitor defining the DC-bus voltage. Although both DC/DC converters can be optimized for their specific task, a disadvantage seems that the battery can not be used to store significant amounts of regenerated energy (downhill driving). This is partly covered by a switch in parallel with the diode, but closing this switch disables the ability to control the battery and the supercapacitor independently.
- In [38, 39], a switched multi-power source approach is considered, which has some similarity with the interleaved multiple-input power converter of [42, 43] and the three-port for battery and supercapacitor in [96].
- As brake, [93] proposes a controlled electric resistor between the nodes of the DC-bus.
- In [106], the supercapacitor is connected via its own DC/DC converter to the input of the DC/DC converter of the fuel cell stack instead of to the DC-bus.
- A further generalization of topologies is found in [19], where DC/DC converters are considered between all elements in the propulsion system, including auxiliaries.

Discussions on different topologies are found in [70, 109]. A discussion on the differences between topology (1) and (2) for a supercapacitor as storage is raised in [83]. In [90], topology (4) with a supercapacitor as storage is compared with topology (2) with a battery as storage. In [70] it is concluded that for a battery as energy storage, topology (2) prevails with respect to a minimum fuel consumption.

Some publications do not state a topology of the propulsion system [20, 111] and discuss their EMS entirely on power level [11, 15, 71], including the properties of possible converters in their characterization of the fuel cell system or storage.

5 Energy Management Strategies

This section intends to provide an overview of presented EMSs for FCHEV, categorized per applied control theory. As presented EMSs occasionally combine different control theories and as control theories themselves are sometimes hard to categorize, these categories should be considered an indication only.

5.1 Classic control

With classic control we refer to linear feed-back/feedforward control as PID-controllers. Within this category, there is a group of publications discussing a power converter on the level

of its electric components (as MOSFETs and IGBTs). As their focus is the discussion of the presentation power converter, a linear controller is included as EMS just to enable a proper operation of the considered converter [40, 96]. Generally, these publications do not consider control goals as a minimum fuel consumption.

The three-port power converter for battery and supercapacitor in [96, 97], includes an EMS implemented as (adaptive) PI-controllers, controlling the duty cycle of the semiconductor power switches. [7] provides a setpoint for a supercapacitor current, based on voltages in the system and a master PI controller. Setpoints are realized using slave PI-controllers. The approach to use the voltage of the supercapacitor as indicator of the amount of stored energy, is also applied in [87, 88], sometimes explicitly referred to as voltage control [75]. A comparable approach, extended to a battery, is presented in [68, 72]. A voltage control approach with a combined converter for fuel cell stack and supercapacitor is demonstrated in [48].

Also on power converter level, an H_{∞} -controller balancing performance and robustness of the converter is discussed in [44]. Distinguishing between three modes of operation, [4] combines PI-control with sliding mode control to distribute transients over the different power sources.

When representing demanded torque and currents in the system as states, linear transfer functions can represent the system components, enabling a linear controller design. Such approach based on states also enables methods as state estimators and state feedback controllers [36].

Where classic control is dedicated to linear relations, flatness-based control can partly deal with nonlinearities in the system, still enabling linear control [73, 74, 92, 91].

5.2 Filtering

Two approaches focussing on wavelet decomposition are presented in [94] for a fuel cell/supercapacitor hybrid and in [107] for a fuel cell/battery/supercapacitor hybrid. These strategies focus on the distribution of the transients in the power demand. [3] combines wavelet decomposition with a small neural network, relating power demand and SOC to the power requested from the fuel cell stack.

Also [61] focusses on frequency content, but implements this on the level of the DC/DC converter using linear transfer functions. [6, 8] discuss an approach that also results in a power split over a frequency range, including the boundaries of the fuel cell stack and the supercapacitor. This approach results in a direct duty cycle control of the DC/DC converter between the supercapacitor and the DC-bus.

5.3 Heuristic strategies

Heuristic strategies do not derive an EMS from a general control theory, but rely on one or a set of heuristic rules to operate the system.

An example of such rule is presented in [1], where the reference for the fuel cell power equals the power demand plus a constant times the deviations in the SOC of the battery. A slightly more complex rule is presented in [108, 109], where a power split ratio between fuel cell stack power and battery power is defined based on the voltage of the fuel cell stack and the SOC of the battery. Such relations can be implemented using lookup tables [98]. [81] directly relates the SOC of the battery to an operating mode of the fuel cell stack, and extends this by shifting the point of operation of the fuel cell stack based on the observed efficiency of the system. As the SOC of the battery is not directly available as measurement, [50] proposes a rule using the open-clamp voltage of the battery to define the reference for the fuel cell stack current.

Under the assumption the battery can deliver power faster than the fuel cell stack, [89] focusses on controlling the battery, deriving the fuel cell stack current from the determined bat-tery current, including a rate limiter on the fuel cell stack current in order to avoid fast changes in the fuel cell current. The reference for the battery current is derived from the DC-bus voltage. This approach is extended to fuel cell/battery/supercapacitor hybrids in [90].

A group of heuristic EMSs consider a set of operating modes. For a fuel cell/supercapacitor hybrid, such a rule based approach differentiating to modes of operation (as braking or delivering peak power), is presented in [29, 34, 71]. Such rules provide setpoints for operation, controlled by local PI controllers [29, 34]. In addition to these rules, the operating set-point per mode can be optimized with respect to a minimum fuel consumption. The number of modes, sometimes referred to as states, may vary. By example, for a fuel cell/battery hybrid, [46] differentiates between six modes of operation, where [45] uses four modes. For a fuel cell/battery/supercapacitor hybrid, [39] uses seven modes to switch on and off the different power sources.

Advantage of most heuristic EMSs is their simplicity and focus on real-time implementation. Disadvantage is that, due to their nature, no guarantees can be provided on properties as stability or the ability to minimize the fuel consumption.

5.4 Fuzzy Control

Popular in the nineties of the last century, fuzzy control provides a linguistic way to create control systems. Compared to other control applications, fuzzy control is relatively frequently presented as approach to obtain an EMS for FCHEVs. This might be caused by the freedom in the system. As example: the amount of stored energy should be kept within the boundaries of the storage, whereas the absolute amount of stored energy is less relevant. This relaxes the accuracy of the control goals, which makes the control problem particulary suited for fuzzy control.

Essentially, fuzzy control defines static, nonlinear relations between inputs and outputs. Still, dynamics can be included by referring to variables as an amount of stored energy or a rate of change. Proposed fuzzy control schemes indeed include the SOC of the battery as input variable, as for example in [15, 59, 66, 69, 100]. Where most papers use power and SOC for fuzzyfication, [55] details this to voltages, currents and changes in voltages, considering a supercapacitor as storage. The nonlinear nature of fuzzy controller is explicitly used in [13] to reduce voltage

ripple on power converter level.

The rules in the inference of the fuzzy controller have to be defined by an expert, who also chooses the size of the fuzzy sets. Sets of seven or more membership functions are presented [33, 63, 80, 100], whereas sets of three or four membership functions [47, 56] also provide experimentally validated solutions [57, 62]. Generally, there is a balance between the number of membership functions and the care needed to define each single membership function. Still, a large number of membership functions increases the complexity of the inference, reducing its maintainability. To adapt to the driving pattern, [80] proposes to relate the position of the membership functions to the current operating conditions. In [56], the position of the membership functions is treated as an optimization problem, maximizing the efficiency of the propulsion system. An adaptive neuro-fuzzy inference system to improve the fuel

economy of the vehicle is presented in [59]. Where [59] combines a small neural network with a fuzzy inference, [23, 24, 25] combine fuzzy control with wavelet filtering to split the power demand over fuel cell stack, battery and supercapacitor. A combination of fuzzy control and flatness control is presented in [106], where a flatness control algorithm decides on the power split between the fuel cell stack and a battery/supercapacitor combination, and within this combination, the fuzzy controller distributes the power over the battery and the supercapacitor. Common to all fuzzy control schemes is that a

real-time implementation is easily obtained. This is an advantage for more complex topologies comprising a fuel cell stack, battery and supercapacitors [33, 58, 66].

Optimizing strategies

As discussed in section 5.4, when there is freedom left in a controlled system, there is room for optimization. Optimizing strategies mathematically define control goals in a cost function, including constraints as power and energy ratings and a constraint on the average stored energy over a driving cycle. The cost function itself generally refers to a minimum in fuel consumption [77, 84, 86], a minimum in costs [104], a minimum in losses [85], or a combination of objectives [41, 42, 43]

Although comparable in their definition of the cost function, various approaches to obtain an optimal control are presented.

A number of papers propose numerical solutions, as Dynamic Programming (DP), nonlinear programming and variations as Stochastical Dynamic Programming (SDP) [51, 53, 54, 78, 82]. One SDP related optimization method including probability is referred to as ant colony optimization [76]. A second SDP related method, intended to approach the global optimum solution efficiently, is referred to as particle swarm optimization [41, 42, 43].

Disadvantage of DP-based solutions is the computational effort needed, possibly hindering real-time implementation. As solution [101, 104] simplifies its DP strategy by considering solutions per driving mode. By representing the cost function as a quadratic function [21, 22, 18, 105], a Linear Quadratic Control (LQC) approach is enabled. In [52], such approach is combined with

a-priori road trip information.

A method originating from Internal Combustion Engine (ICE) based hybrid propulsion systems, is the Equivalent Cost Minimization Strategy (ECMS). A number of publications discuss the application of ECMS to FCHEVs [79, 93, 103]. ECMS characterizes engine and storage with first or second order polynomials to enable a global minimum. Some variations are presented combining ECMS with a prediction [35] or estimation of the power demand and transient load of

the fuel cell stack [102].

The approximation of first principle models with polynomials is not necessary for fuel cell hybrids with a battery as storage, as the first principle characterization of the fuel cell stack and the battery have mathematically congruent representations. As a result, an EMS providing a global minimum can be derived based on the first principle models directly [84, 86]. Such analytical solutions based on Pontryagin's Maximum/Minimum Principle or Bellman's principle of optimality, provide real-time implementable solutions, still approaching optimality [86, 111]. Such optimal solution is even reduced further in complexity to a rule based EMS in [110, 112]. Still, to provide a solution, information is needed on the future behavior of the vehicle, typically to define the value of the Lagrange multiplier(s) in the optimization. In [11, 85] this Lagrange multiplier is related to the energy content of the battery. The need for this information is reduced to an estimate of the future average power demand, based on the past power demand, represented by the SOE of the battery in [85, 86]. In [84, 86], this is reduced to the current demand, represented by the SOC of the battery. An adapting algorithm estimating such future system behavior is proposed in [60], a heuristic prediction is presented in [14] and a-priori trip information is included in [52].

Model Predictive Controllers (MPC) predict the future, based on a model of the system. Such approach, including a quadratic cost function and system identification based on multiple models, is presented in [16]. Also [2] proposes to distribute the operating area of the propulsion system over a set of linear models and combines this with an MPC approach.

5.6 Maximizing efficiency

To obtain a minimum fuel consumption, a number of papers focus on the efficiency of the fuel

cell system [17, 19, 26, 95]. Based on a map of the fuel cell system efficiency, zones are defined with a mode of operation per zone as EMS [30, 31]. Also [12] defines modes by thresholds, and operates the fuel cell stack on its maximum efficiency in one of these modes. Essentially, these approaches are based on static considerations on the efficiency. In [20] such approach is combined with an adaptive controller to cover transients in the operation of the fuel cell system, attempting to maximize the efficiency of the fuel cell system dynamically.

When designing an EMS on efficiency maps, it should be noted that the maximum efficiency of the fuel cell stack does not necessarily match the maximum efficiency of the propulsion system.

6 Discussion

A few studies compare different EMSs. In [27] a PID-based EMS is compared with a fuzzy control based EMS. This is extended with an optimization method in [28], from which it was concluded that the optimization method prevailed with respect to a minimum fuel consumption. For heuristic approaches, [49] examined on/off strategies based on the maximum fuel cell power, on the maximum fuel cell stack efficiency and on a combination of both, for which the combination provided an acceptable balance between efficiency and power. Within optimizing methods, [85] compared a ECMS-based approach with an analytical solution to the optimization problem, where the analytical solution performed best on fuel efficiency, although differences are small.

Classic control theory uses linear models providing appealing properties as guaranteed stability and robustness. As the actual propulsion system is far from linear with respect to fuel consumption and voltage/current relations, a guaranteed minimum fuel consumption can not be expected when linear control theory is applied.

Heuristic strategies and fuzzy control can easily handle nonlinearities, providing, possibly combined with filtering techniques, an appropriate way to control also fuel cell hybrids with both a battery and a supercapacitor as storage. Heuristic rules defining different operating modes do have a risk. For each combination of modes or rules, it should be evaluated if the operation of the system is stable and oscillation when switching between states should be avoided.

When focus is on a minimum fuel consumption, optimizing strategies are preferred. With respect to fuel consumption, real-time implementation and plug-in functionality, an EMS based on an analytical solution to the optimization problem seems to be favorable for systems with only a battery as storage.

From the discussion which EMS optimizes the operation of a FCHEVs, naturally follows the discussion which component sizes for fuel cell stack and storage are optimal. A few publications make an observation on this subject [1, 9, 10, 86].

7 Conclusions

For a broad variety of vehicle types and propulsion system topologies, energy management strategies have been presented in literature. Also with respect to optimization goals as a minimum fuel consumption, solutions are presented. Therefore, we can conclude that for most fuel cell hybrid vehicle designs, literature provides an applicable EMS. Thus, compared with a decade ago, the design of an appropriate EMS is no hurdle anymore, hindering the introduction of fuel cell hybrid propulsion systems.

With respect to the validation of EMSs and considered topologies, only a minority of the presented work is reported to be validated on a fuel cell hybrid vehicle. Experiments and applied research can further elucidate the value of the proposed EMSs.

From a scientific standpoint, some subjects are interesting for further research. Especially with respect to optimizing strategies, possible information on the future driving cycle might further reduce the fuel consumption. Here, we can consider a prediction of the future driving cycle based on navigation data, dynamic route information or on statistical trip information. With respect to the propulsion system, using advanced models, issues as battery and fuel cell stack aging can be included in the optimization problem, extending the lifetime of the propulsion system. In addition, an extension of the area of operation to harsh environments and cold startups is interesting to increase the robustness of the fuel cell hybrid propulsion system.

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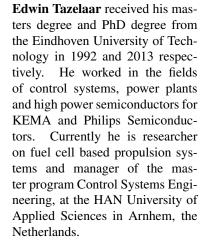
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Authors





Bram Veenhuizen received his masters degree and PhD degree from the University of Amsterdam in 1984 and 1988 respectively. He joined SKF focussing on electromagnetic and X-ray techniques to characterize materials and material fatigue. In 1995 he joined van Doornes Transmisie, where he was responsible for the realization of some advanced drive train projects. In 2002 he was appointed assistant professor at the Eindhoven University of Technology. Since 2005 he is professor in vehicle mechatronics at the HAN University of Applied Sciences.



José Jagerman received her bachelor degree from the Library and Documentation Academy in 1987. For several years, she worked at the library of the Police Academy. Currently she is working as a librarian at the Studycentre of HAN University of Applied Sciences in Arnhem, the Netherlands.



Ton Faassen has followed a number of trainings at GO Educations, School of Information. From 1994, he worked at the library of Automotive and Engineering. Currently he is working as a librarian at the Studycentre of HAN University of Applied Science in Arnhem, the Netherlands.

